

# Chapter 9: FET Amplifiers And Switching Circuits

## 9-1: The Common Source Amplifier (CS Amplifier)

FET has an important advantage compared to the BJT due to the FET's extremely high input impedance. Disadvantages, however, include higher distortion and lower gain. The common-source (CS) amplifier is incomparable to the common-emitter BJT amplifier that you studied in Chapter 6.

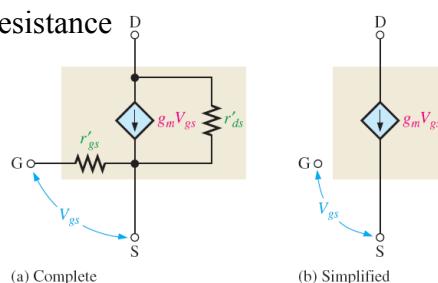
**FET AC Model:** the ac model for FET is shown below

$r'_{gs}$  is the gate source internal resistance

$g_m V_{gs}$  is the current appear between drain and source

$r'_{ds}$  is the internal drain - to - source resistance

Since  $r'_{gs}$  is very large and  $r'_{ds}$  is also large → they can be neglected  
→ Simplified model



## 9-1: The Common Source Amplifier

### FET AC Model

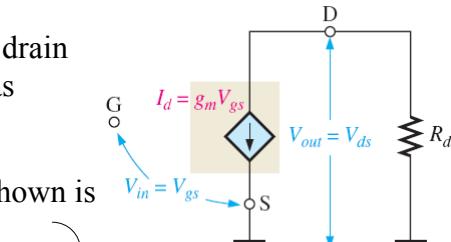
An ideal ac circuit model with ac drain resistance  $R_d$  can be represented as shown.

The voltage gain for the circuit shown is

$$A_v = \frac{V_{out}}{V_{in}} = \frac{V_{ds}}{V_{gs}} \quad \left( \begin{array}{l} \text{but } V_{ds} = I_d R_d \\ \text{and } V_{gs} = \frac{I_d}{g_m} \end{array} \right) \quad \text{From definition of transconductance } g_m = I_d/V_{gs}$$

$$\rightarrow A_v = \frac{I_d R_d}{I_d/g_m} = \frac{g_m I_d R_d}{I_d}$$

$\rightarrow A_v = g_m R_d$

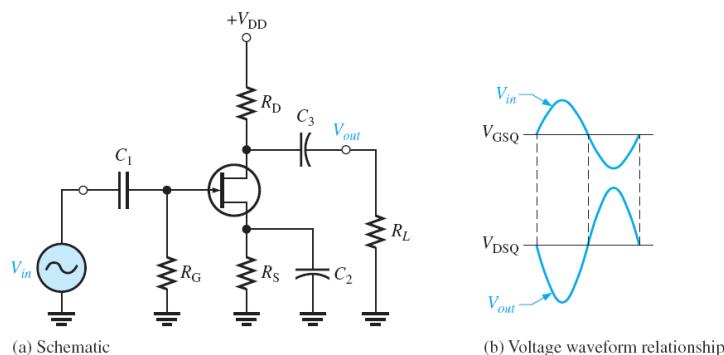


Ex: for a JFET with  $g_m = 4\text{mS}$  and  $R_d = 1.5\text{k}\Omega$   
 → ideal voltage gain is  
 $A_v = g_m R_d = (4\text{mS})(1.5\text{k }\Omega) = 6$

## 9-1: The Common Source Amplifier

### JFET Amplifier Operation

In common source self biased amplifier,  $V_{in}$  is applied to the gate and  $V_{out}$  is taken from the drain as shown with phase difference between them  $180^\circ$

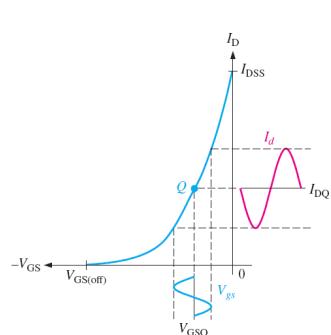


Remember that, for ac signal, capacitors are short and  $V_{DD}$  is ac ground → source terminal  $S$  and  $R_D$  are connected to the round in ac equivalent circuit

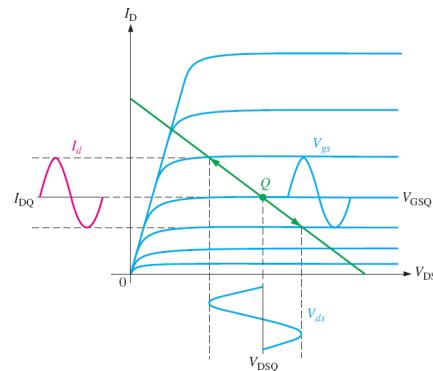
## 9-1: The Common Source Amplifier

### JFET Amplifier Operation: A Graphical Picture

the operation of n-channel JFET shown above with  $V_{in}$  and  $V_{out}$  on  $I_D$  characteristic curve and on transfer characteristic curve is shown below



(a) JFET (n-channel) transfer characteristic curve showing signal operation



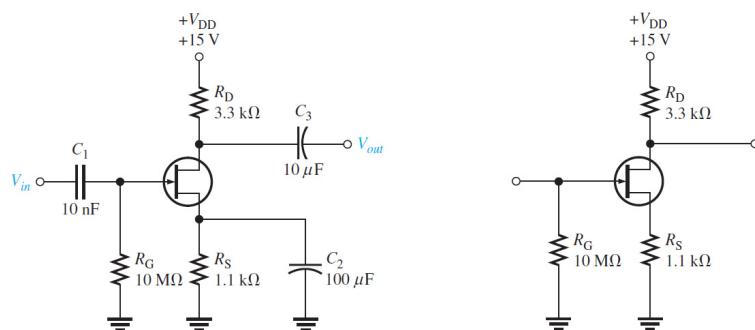
(b) JFET (n-channel) drain curves showing signal operation

As  $V_{gs}$  varies  $\rightarrow I_d$  varies; As  $V_{gs}$  decrease (more negative) from Q-point  $\rightarrow I_d$  decreases and As  $V_{gs}$  increase  $\rightarrow I_d$  increases. The corresponding change in  $V_{ds}$  show the inverse (because  $V_D = V_{DD} - I_D R_D$ ).

## 9-1: The Common Source Amplifier

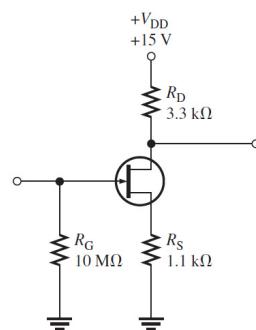
### JFET Amplifier Operation: DC Analysis

From the DC equivalent circuit of the amplifier, the Q-point can be found graphically as described before in chapter 8 for the self biased transistor  
 $\rightarrow$  Once finding  $I_D$  you can find  $V_D$



▲ FIGURE 9-5

JFET common-source amplifier.



▲ FIGURE 9-6

DC equivalent for the amplifier in Figure 9-5.

## 9-1: The Common Source Amplifier

### JFET Amplifier Operation: DC Analysis: Example

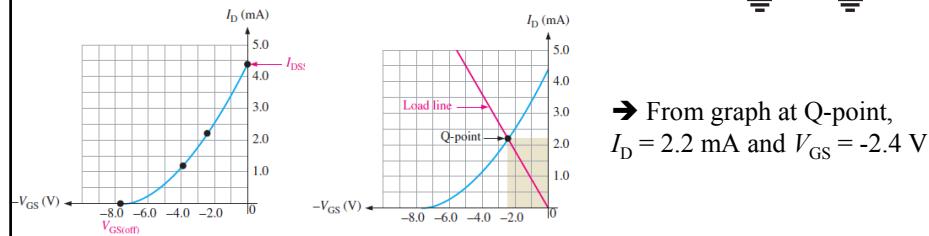
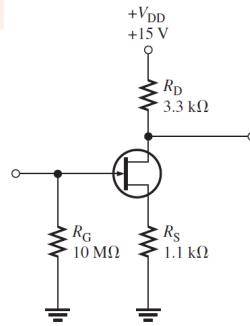
Determine  $I_D$  and  $V_{GS}$  at the  $Q$ -point for the JFET amplifier in Figure 9–6. The typical  $I_{DSS}$  for this particular JFET is 4.3 mA and  $V_{GS(off)}$  is  $-7.7$  V.

Plot the transconductance curve

$$V_{GS} = 0.3V_{GS(off)} = -2.31 \text{ V} \quad \text{when } I_D = \frac{I_{DSS}}{2} = 2.15 \text{ mA}$$

$$V_{GS} = 0.5V_{GS(off)} = -3.85 \text{ V} \quad \text{when } I_D = \frac{I_{DSS}}{4} = 1.075 \text{ mA}$$

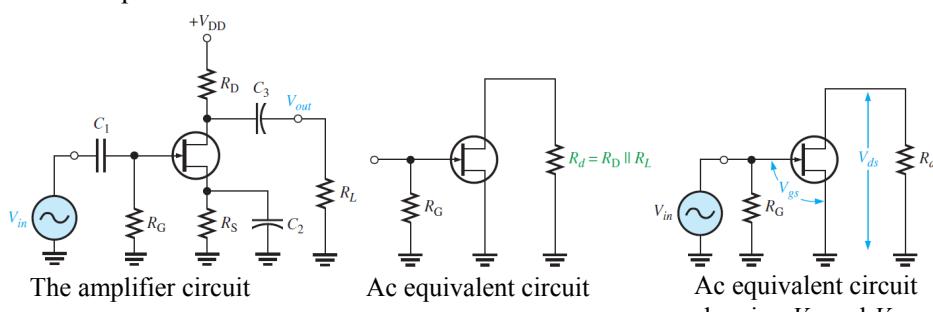
Draw the load line from the two points first point ( $I_D=0$  and  $V_{GS} = 0$ ) and the second point  $I_D = I_{DSS}$  and  $V_{GS} = -I_D R_S$



## 9-1: The Common Source Amplifier

### JFET Amplifier Operation: AC Analysis

The ac equivalent circuit can be drawn



#### Input resistance

$$R_{in} = R_G \parallel \left( \frac{V_{GS}}{I_{GSS}} \right) \approx R_G$$

Very small

#### Output resistance

$$R_{out} = R_d$$

with no  $R_L \rightarrow R_d = R_D$

With load  $R_L \rightarrow R_d = R_D // R_L$

#### Voltage gain

$$A_v = \frac{V_{out}}{V_{in}} = \frac{V_{ds}}{V_{in}} = g_m R_d$$

## 9-1: The Common Source Amplifier

### JFET Amplifier Operation: AC Analysis - Example

What is the total output voltage for the unloaded amplifier in Figure 9-9?  $I_{DSS}$  is 4.3 mA;  $V_{GS(\text{off})}$  is -2.7 V;  $I_{DQ}$  = 1.91 mA. If a 4.7 k $\Omega$  load resistor is ac coupled to the output of the amplifier what is the resulting output voltage?

$$V_D = V_{DD} - I_D R_D = 12 \text{ V} - (1.91 \text{ mA})(3.3 \text{ k}\Omega) = 5.70 \text{ V}$$

Next calculate  $g_m$

$$V_{GS} = -I_D R_S = -(1.91 \text{ mA})(470 \Omega) = -0.90 \text{ V}$$

$$g_{m0} = \frac{2I_{DSS}}{|V_{GS(\text{off})}|} = \frac{2(4.3 \text{ mA})}{2.7 \text{ V}} = 3.18 \text{ mS}$$

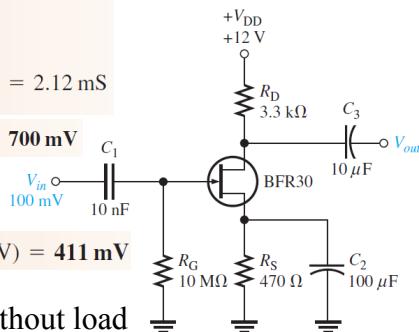
$$g_m = g_{m0} \left( 1 - \frac{V_{GS}}{V_{GS(\text{off})}} \right) = 3.18 \text{ mS} \left( 1 - \frac{-0.90 \text{ V}}{-2.7 \text{ V}} \right) = 2.12 \text{ mS}$$

$$V_{out} = A_v V_{in} = g_m R_D V_{in} = (2.12 \text{ mS})(3.3 \text{ k}\Omega)(100 \text{ mV}) = 700 \text{ mV}$$

If a 4.7 k $\Omega$  load resistor is ac coupled to the output of

$$V_{out} = A_v V_{in} = g_m R_d V_{in} = (2.12 \text{ mS})(1.94 \text{ k}\Omega)(100 \text{ mV}) = 411 \text{ mV}$$

Voltage gain with load < voltage gain without load



## 9-1: The Common Source Amplifier

### JFET Amplifier Operation: AC Analysis - Example

What input resistance is seen by the signal source in Figure 9-11?  $I_{GSS} = 30 \text{ nA}$  at  $V_{GS} = 10 \text{ V}$ .

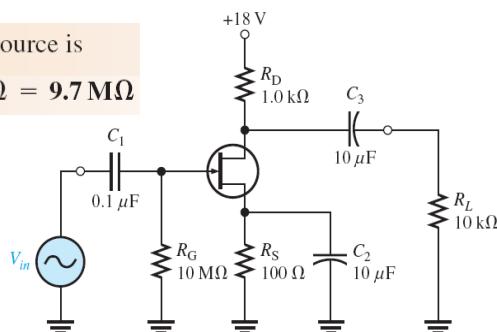
The input resistance at the gate of the JFET is

$$R_{IN(\text{gate})} = \frac{V_{GS}}{I_{GSS}} = \frac{10 \text{ V}}{30 \text{ nA}} = 333 \text{ M}\Omega$$

The input resistance seen by the signal source is

$$R_{in} = R_G \parallel R_{IN(\text{gate})} = 10 \text{ M}\Omega \parallel 333 \text{ M}\Omega = 9.7 \text{ M}\Omega$$

$$\rightarrow R_{in} \approx R_G$$



## 9-1: The Common Source Amplifier

### D-MOSFET Amplifier Operation:

- A zero-biased common-source amplifier for *n*-channel D-MOSFET is shown.

- $V_{GS} = 0 \rightarrow$  The signal voltage causes  $V_{gs}$  to swing above and below its zero value, producing a swing in  $I_d$  above and below Q-point, as shown on characteristic transfer curve

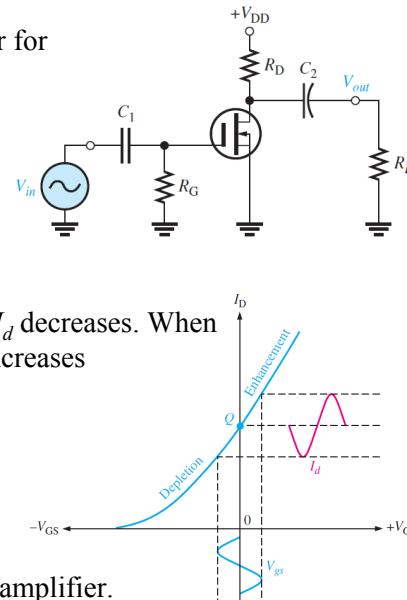
When  $V_{gs} < 0 \rightarrow$  the depletion mode, and  $I_d$  decreases. When  $V_{gs} > 0 \rightarrow$  the enhancement mode, and  $I_d$  increases

At  $V_{GS} = 0 \rightarrow I_D = I_{DSS}$

$\rightarrow V_D = V_{DS}$  can be calculated

$$V_D = V_{DD} - I_D R_D$$

The ac analysis is the same as for the JFET amplifier.



## 9-1: The Common Source Amplifier

### E-MOSFET Amplifier Operation:

- A voltage divider common-source amplifier for *n*-channel E-MOSFET is shown.

- The gate is biased with a positive voltage such that  $V_{GS} > V_{GS(th)}$

- Dc analysis  $V_{GS} = \left( \frac{R_2}{R_1 + R_2} \right) V_{DD}$

$$I_D = K(V_{GS} - V_{GS(th)})^2$$

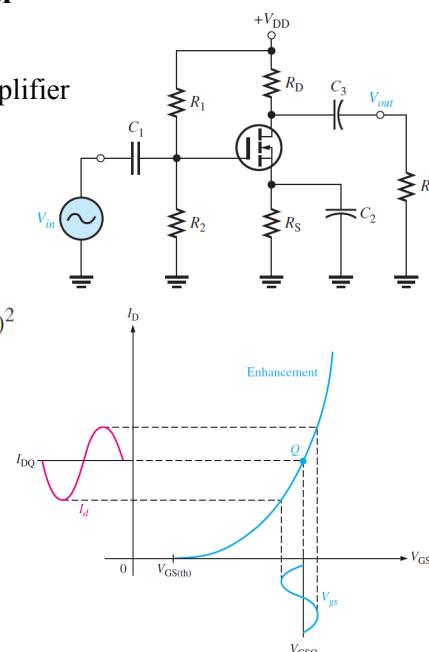
$$V_{DS} = V_{DD} - I_D R_D$$

- Ac analysis  $R_{in} = R_1 \parallel R_2 \parallel R_{IN(gate)}$

$$\text{where } R_{IN(gate)} = V_{GS}/I_{GSS}$$

- Voltage gain is same as for JFET

$$A_v = \frac{V_{out}}{V_{in}} = \frac{V_{ds}}{V_{gs}} = g_m R_d$$



## 9-1: The Common Source Amplifier

### E-MOSFET Amplifier Operation: Example

A common-source amplifier using an E-MOSFET is shown in Figure 9-17. Find  $V_{GS}$ ,  $I_D$ ,  $V_{DS}$ , and the ac output voltage. Assume that for this particular device,  $I_{D(on)} = 200 \text{ mA}$  at  $V_{GS} = 4 \text{ V}$ ,  $V_{GS(th)} = 2 \text{ V}$ , and  $g_m = 23 \text{ mS}$ .  $V_{in} = 25 \text{ mV}$ .

$$V_{GS} = \left( \frac{R_2}{R_1 + R_2} \right) V_{DD} = \left( \frac{820 \text{ k}\Omega}{5.52 \text{ M}\Omega} \right) 15 \text{ V} = 2.23 \text{ V}$$

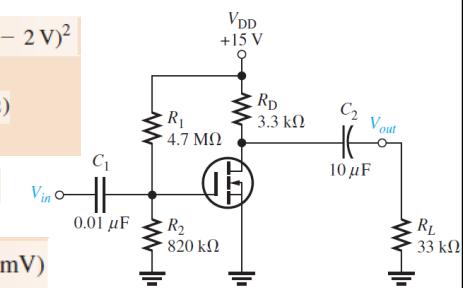
$$\text{For } V_{GS} = 4 \text{ V}, \quad K = \frac{I_{D(on)}}{(V_{GS} - V_{GS(th)})^2} = \frac{200 \text{ mA}}{(4 \text{ V} - 2 \text{ V})^2} = 50 \text{ mA/V}^2$$

$$\rightarrow I_D = K(V_{GS} - V_{GS(th)})^2 = (50 \text{ mA/V}^2)(2.23 \text{ V} - 2 \text{ V})^2 \\ = 2.65 \text{ mA}$$

$$V_{DS} = V_{DD} - I_D R_D = 15 \text{ V} - (2.65 \text{ mA})(3.3 \text{ k}\Omega) \\ = 6.26 \text{ V}$$

$$R_d = R_D \parallel R_L = 3.3 \text{ k}\Omega \parallel 33 \text{ k}\Omega = 3 \text{ k}\Omega$$

$$V_{out} = A_v V_{in} = g_m R_d V_{in} = (23 \text{ mS})(3 \text{ k}\Omega)(25 \text{ mV}) \\ = 1.73 \text{ V}$$



## 9-2: The Common Drain Amplifier (CD Amplifier) or source follower

■ In a CD amplifier, the input signal is applied to the gate and the output signal is taken from the source. There is no drain resistor, because it is *common* to the input and output signals.

■ The voltage gain is

$$A_v = \frac{V_{out}}{V_{in}} = \frac{V_s}{V_{gs} + V_s} = \frac{I_d R_s}{V_{gs} + I_d R_s} = \frac{g_m V_{gs} R_s}{V_{gs} + g_m V_{gs} R_s}$$

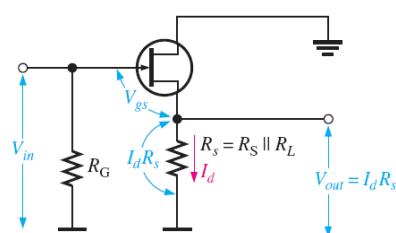
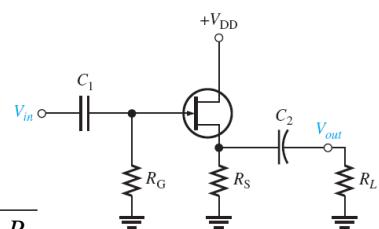
$$\rightarrow A_v = \frac{g_m R_s}{1 + g_m R_s}$$

$$\text{If } g_m R_s \gg 1 \rightarrow A_v \approx 1$$

### Input Resistance

$$R_{in} = R_G \parallel R_{IN(gate)}$$

$$\text{where } R_{IN(gate)} = V_{GS}/I_{GSS}$$



Ac equivalent circuit

## 9-2: The Common Drain Amplifier

### Example

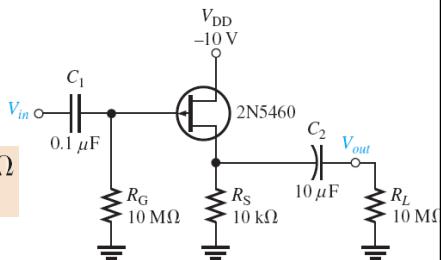
Determine the voltage gain and the input resistance of the amplifier in Figure 9–20.  $V_{DD}$  is negative because it is a *p*-channel device. From data sheet  $g_m = y_{fs} = 1000\mu\text{S}$ ,  $I_{GSS} = 5 \text{ nA}$  (maximum) at  $V_{GS} = 20 \text{ V}$ .

Since  $R_L \gg R_S$ ,  $R_s \cong R_S$

$$\rightarrow A_v = \frac{g_m R_S}{1 + g_m R_S} = \frac{(1000 \mu\text{S})(10 \text{ k}\Omega)}{1 + (1000 \mu\text{S})(10 \text{ k}\Omega)} = 0.909$$

$$R_{IN(gate)} = \frac{V_{GS}}{I_{GSS}} = \frac{20 \text{ V}}{5 \text{ nA}} = 4000 \text{ M}\Omega$$

$$\rightarrow R_{in} = R_G \parallel R_{IN(gate)} = 10 \text{ M}\Omega \parallel 4000 \text{ M}\Omega \cong 10 \text{ M}\Omega$$



## 9-3: The Common Gate Amplifier (CG Amplifier)

- In a CG amplifier, the input signal is applied to the source and the output signal is taken from the drain.

- The voltage gain is

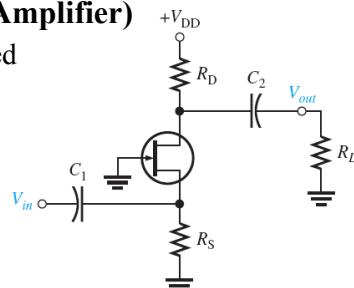
$$A_v = \frac{V_{out}}{V_{in}} = \frac{V_d}{V_{gs}} = \frac{I_d R_d}{V_{gs}} = \frac{g_m V_{gs} R_d}{V_{gs}}$$

$$\rightarrow A_v = g_m R_d \quad \text{where } R_d = R_D \parallel R_L$$

### Input Resistance

$$R_{in(source)} = \frac{V_{in}}{I_{in}} = \frac{V_{gs}}{I_s} = \frac{V_{gs}}{I_d} = \frac{V_{gs}}{g_m V_{gs}} = \frac{1}{g_m}$$

$$\rightarrow R_{in} = R_{in(source)} \parallel R_S$$



### 9-3: The Common Gate Amplifier (CG Amplifier)

#### Example

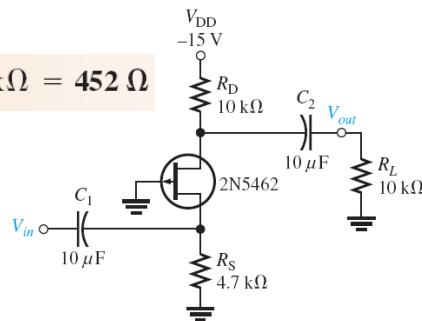
Determine the minimum voltage gain and input resistance of the amplifier in Figure 9–23.  $V_{DD}$  is negative because it is a *p*-channel device.  $g_m = 2000 \mu\text{S}$  minimum

$$A_v = g_m R_d$$

$$\rightarrow A_v = g_m(R_D \parallel R_L) = (2000 \mu\text{S})(10 \text{ k}\Omega \parallel 10 \text{ k}\Omega) = 10$$

$$R_{in(source)} = \frac{1}{g_m} = \frac{1}{2000 \mu\text{S}} = 500 \Omega$$

$$\rightarrow R_{in} = R_{in(source)} \parallel R_S = 500 \Omega \parallel 4.7 \text{ k}\Omega = 452 \Omega$$



### 9-3: The Common Gate Amplifier (CG Amplifier)

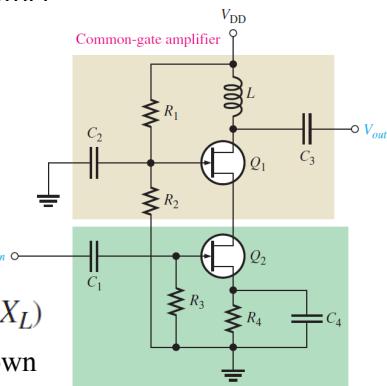
#### The Cascode Amplifier

■ A **cascode** amplifier is one in which a common-source amplifier and a common-gate amplifier are connected in a series arrangement as shown below. As noted from figure, the input resistance ( $1/g_m$ ) for CG amplifier represent the drain resistance  $R_d$  for CS amplifier

■ The cascode amplifier using JFETs provides a very high input resistance and significantly reduces capacitive effects to allow for operation at much higher frequencies, used for RF (radio frequency), than a common-source amplifier alone  
The voltage gain

$$A_v = A_{v(CS)} A_{v(CG)} = (g_{m(CS)} R_d)(g_{m(CG)} X_L)$$

Where  $X_L$  is the reactance of the inductor  $L$  shown



$$\rightarrow A_v = \left( g_{m(CS)} \left( \frac{1}{g_{m(CG)}} \right) \right) (g_{m(CG)} X_L) \cong g_{m(CG)} X_L \quad \text{with } g_{m(CS)} \approx g_{m(CG)}$$

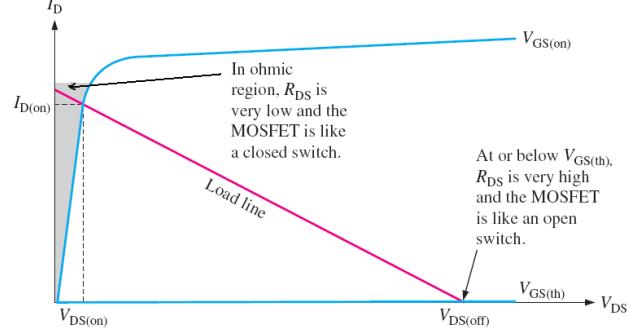
## 9-5: MOSFET Analogue Switching

MOSFETs are widely used in analog and digital switching applications. Generally, they exhibit very low *on*-resistance, very high *off*-resistance, and fast switching times.

### MOSFET Switching Operation

- E-MOSFETs are generally used for switching applications:

- When  $V_{GS} < V_{GS(\text{th})}$  → MOSFET is *off* → very high  $R_{DS}$
- When  $V_{GS} > V_{GS(\text{th})}$  → MOSFET is *on* → very low  $R_{DS}$  ( $V_{GS}$  must be sufficiently higher than  $V_{GS(\text{th})}$  to be in the upper end of load line in the Ohmic region)



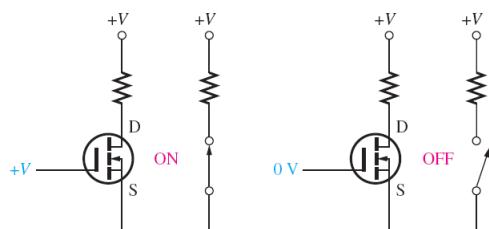
## 9-5: MOSFET Analogue Switching

### MOSFET Switching Operation

- n-channel E-MOSFET operation as a switch

$V_{GS}$  is  $+V$  → switch on

$V_{GS}$  is  $0$  → switch off

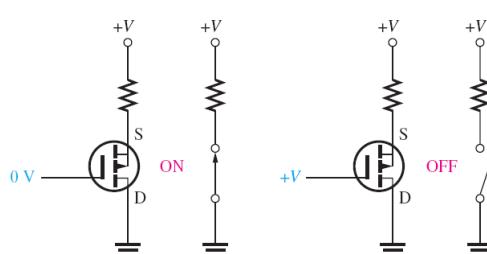


(a) n-channel MOSFET and switch equivalent

- p-channel E-MOSFET operation as a switch

$V_{GS}$  is  $0$  → switch on

$V_{GS}$  is  $+V$  → switch off

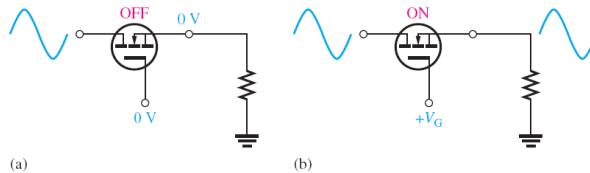


(b) p-channel MOSFET and switch equivalent

## 9-5: MOSFET Analogue Switching

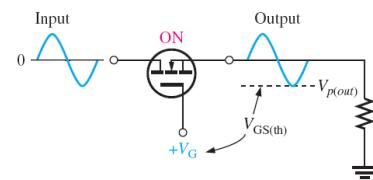
### The analogue switch

- A basic *n*-channel MOSFET **analog switch** is shown in the figure. The signal at the drain is connected to the source when the MOSFET is turned on by a positive  $V_{GS}$  and is disconnected when  $V_{GS}$  is 0, as indicated.



(a) (b)

- Variable voltage at the source cause variation in  $V_{GS} \rightarrow V_{GS}$  must be  $\geq V_{GS(th)}$  to keep MOSFET maintain conduction (on). Minimum  $V_{GS}$  voltage occurs at -ve peak voltage of the output ( $V_{p(out)}$ )



$$V_{GS} = V_G - V_{p(out)} \geq V_{GS(th)}$$

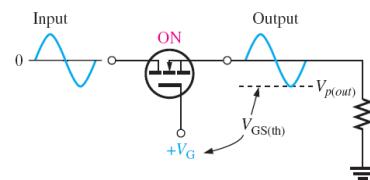
## 9-5: MOSFET Analogue Switching

### The analogue switch: Example

A certain analog switch similar to the one shown in Figure 9-35 uses an *n*-channel MOSFET with  $V_{GS(th)} = 2$  V. A voltage of +5 V is applied at the gate to turn the switch *on*. Determine the maximum peak-to-peak input signal that can be applied, assuming no voltage drop across the switch.

The difference between the gate voltage and the negative peak of the signal voltage must equal or exceed the threshold voltage. For maximum  $V_{p(out)}$ ,

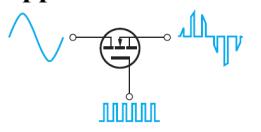
$$\begin{aligned} V_G - V_{p(out)} &= V_{GS(th)} \\ V_{p(out)} &= V_G - V_{GS(th)} = 5\text{ V} - 2\text{ V} = 3\text{ V} \\ V_{pp(in)} &= 2V_{p(out)} = 2(3\text{ V}) = 6\text{ V} \end{aligned}$$



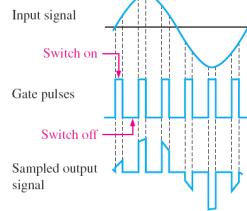
## 9-5: MOSFET Analogue Switching

### The analogue switch: some applications

- Sampling circuit: analogue to digital conversion

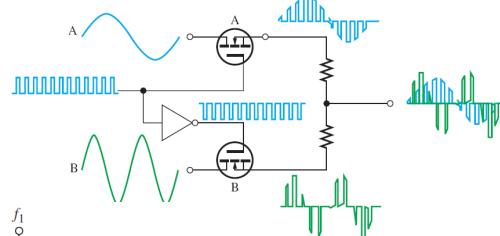


(a) Circuit action

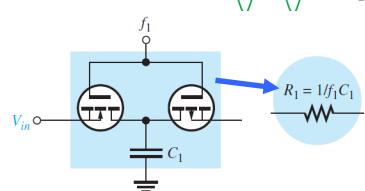


(b) Waveform diagram

- Analogue multiplexer: two or more signals are to be routed to the same output



- Switched-Capacitor Circuit: where switch MOSFETs with a capacitor can be used to replace a resistor

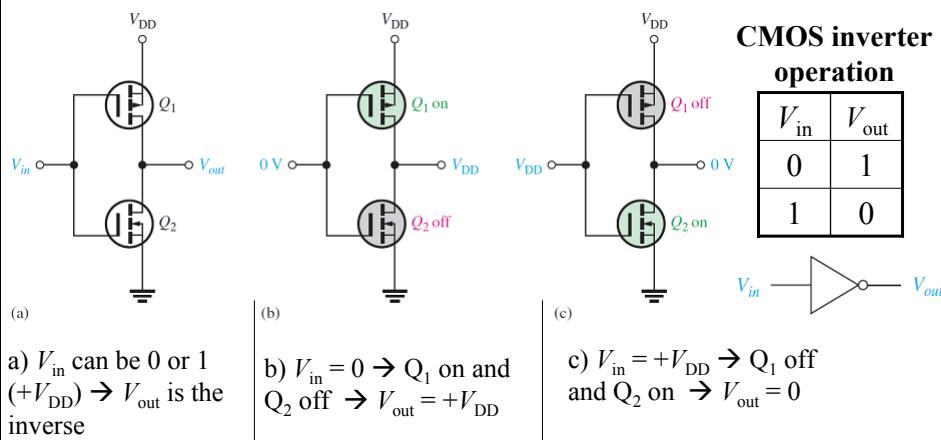


## 9-5: MOSFET Digital Switching

MOSFETs are also used in switching applications in digital integrated circuits

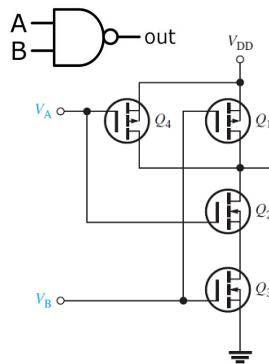
### CMOS (Complementary MOS)

CMOS combines *n*-channel and/or *p*-channel E-MOSFETs in a series arrangement. The shown figure represent a logic **Inverter Gate**



## 9-5: MOSFET Digital Switching

### CMOS (Complementary MOS): *NAND* Gate and *NOR* Gate



**■ NAND Gate:**  
When  $V_A$  AND  $V_B$  are high, the output is low; otherwise, the output is high.

$V_A$	$V_B$	$Q_1$	$Q_2$	$Q_3$	$Q_4$	$V_{out}$
0	0	on	off	on	off	$V_{DD}$
0	$V_{DD}$	off	on	on	off	$V_{DD}$
$V_{DD}$	0	on	off	off	off	$V_{DD}$
$V_{DD}$	$V_{DD}$	off	on	on	off	0

$V_A$	$V_B$	$Q_1$	$Q_2$	$Q_3$	$Q_4$	$V_{out}$
0	0	on	off	on	off	$V_{DD}$
0	$V_{DD}$	off	on	on	off	0
$V_{DD}$	0	on	off	on	off	0
$V_{DD}$	$V_{DD}$	off	on	off	on	0

**■ NOR Gate:**  
When  $V_A$  OR  $V_B$  OR both are high, the output is low; otherwise, the output is high.

